Plot 5000 Hatfield Business Park

Flood Risk Assessment & Drainage Strategy

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REPORT STATUS

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1 Introduction

This Flood Risk Assessment has been prepared on behalf of Goodman UK Ltd, in support of a planning application for a proposed new B1c, B2, or B8 development at Plot 5000, Hatfield Business Park, Hatfield.

Plot 5000 is located off Mosquito Way north west of the roundabout junction with Dragon Road and Tamblin Way and is largely an undeveloped parcel of green land.

The development site has an approximate area of 1.2 hectares in total and an O.S. grid reference of E521274, N209100. A site location plan is included within appendix A of this report.

Although Plot 5000 is undeveloped it can be said that the remaining business park is well developed and operational with a varying complexity of businesses currently residing at the park.

This assessment has been prepared following the guidance set out in National Planning Policy Framework (NPPF) formerly Planning Policy Statement Note no. 25.

Further guidance has been obtained from:

- EA / DEFRA R&D document W5-74/A/TR/1 "Preliminary rainfall runoff for new developments" Revision D, including figures 2.1 & 2.2.
- o "Interim National Procedures" point 3, 10.2 & 10.3
- o The Suds Manual (c753)
- o "Interim Code of Practice for Sustainable Drainage Systems 2004" (ICOP SUDS).

2 Existing Site

2.1 Site Location and Receiving Watercourse / River

The existing site is 100% soft landscaped and currently has no formal positive drainage system on-site discharging to off-site watercourses.

The current Hatfield Business Park development has a park wide adopted infrastructure foul and surface water drainage system that was implemented as part of the redevelopment of the historic Hatfield Aerodrome site during the late 1990's and early 2000's.

This drainage system has been designed to cater for all future plot developments at the business park and has previously been signed-off and approved by the local authority and The Environment Agency.

The existing surface water system generally comprises a network of oversized sewers located beneath the main infrastructure spine roads to the business park.

The surface water sewer sizes range between 1350 – 2400mm in diameter and provide the necessary attenuation volume required to limit discharge rates from the park to Greenfield run-off rates.

Flows from the sewers are discharged to the Ellenbrook receiving watercourse and are controlled / limited by an existing storm water pumping station.

Further attenuation volume is also provided by a series of off-line balancing ponds that at located adjacent to the Ellenbrook Watercourse.

2.1.1 Topography

The existing levels of Plot 5000 vary from between 74.43m AOD to the eastern boundary to 75.54m AOD to the south east corner of the site. (Refer to the topographical survey plan within appendix A).

2.1.2 Description of Catchment

The Environment Agency flood plain map confirms the application site is <u>not</u> within a recognised floodplain and is categorised as Flood Zone 1.

2.2 Geology

A Desk Top Study Report has been carried out by RSK Environment Ltd over the extent of the site. This study includes:

- Groundsure Geo Insight geo-environmental information.
- Trial pits of varying depth upto 3.7m deep.
- Drainage Infiltration / soakaway testing.
- CBR % Testing

Their findings are as follows:

Published geological records for the site indicate that it is underlain by superficial drift deposits of the Lowestoft Formation comprising of clays, clayey sands and gravels, silts and fine to course flint.

Preliminary trial pit data has been issued and is included within Appendix D of this report, it can be summarised as follows:

Strata Thickness	Strata Description
0.0 – 0.3m	TOPSOIL comprising clay with occasional roots, gravelly clayey sand.
0.0 – 0.5m	MADE GROUND comprising grass over sandy clay with occasional roots, gravel also observed along with angular flint and brick fragments.
0.15 – 1.80m	CLAY, silty sandy slightly gravelly with course sand. Gravel is angular fine to course flint.
0.5 – 3.30m	SAND, fine to course, gravel in angular to sub-rounded fine to course flint.
2.20 – 3.30m	GRAVEL, orange grown slightly silty and clayey. Sand is coarse. Gravel is angular to sub-rounded fine to coarse flint.

Soil infiltration soakaway have been carried out at the site, and confirms permeability vary from 5.13 x 10^{-6} m/s to 2.92 x 10^{-5} m/s (refer to appendix D)

Groundwater was encountered only in TP05 with seepage occurring 3.10m bgl.

CBR % testing was carried out in six locations (refer to appendix D for results of tests).

3 Flood Risk Assessment (Pre Development)

3.1 Existing Information on Flood Risk

3.1.1 Tidal/Coastal

Tidal or coastal flooding is not considered a risk as the nearest coast is approx. 63 kilometres away from the site.

3.1.2 Groundwater

Groundwater flooding is not known to be an issue. The existing site has had no problem with any form of groundwater, only on trial pit (TP05) encountered groundwater at a depth of 3.10m bgl. (Refer to trial pits in appendix D).

3.1.3 Surface Water

There is no evidence to suggest that the site currently drains to the existing adopted surface water sewers in the vicinity. Discharge from the development into the public sewer in Mosquito Way is proposed and is to be approved by Thames Water and the Environment Agency in line with historic approvals already in place.

3.1.4 Rivers / Watercourses

The Environment Agency publishes floodplain the internet maps on (http://www.environment-agency.gov.uk). These maps show the possible extent of fluvial flooding for the 1 in 100-year flood (that which would have a 1% probability of being exceeded each year) or the possible extent of tidal flooding to a 1 in 200 year event. A plan showing the extent of the flooding along the nearest marked Environment Agency marked watercourse is presented in appendix A. This plan shows that the development under consideration is outside the area of any recognised floodplain.

4 Proposed Site

4.1 Description of development

The proposed planning application is for the development of a B1c, B2 or B8 building (subject to confirmation) of approximately 4,780 sq.m with a two-storey office facility of 1,550 sq.m.

The development site area is approximately 1.20 hectares.

The proposed building will have a two level access door to its main elevation with level entry doors to the warehouse and office main entrance. (Subject to detail design).

The external areas will comprise an access road, service yard, car parking including HGV manoeuvring space.

A soft Landscape scheme will also be integrated into the proposed development.

Development external levels strategy will seek to (where possible) follow the contours of the existing site so as to minimise the requirement for any retaining walls.

Proposed development levels will also be set such that should any flooding occur it is controlled and kept within the new development demise and not affect neighbouring properties or highway land.

5 Drainage Strategy

5.1 Existing Drainage

The existing site is currently an undeveloped "green" site that does not discharge surface water by means of any positive drainage system to off-site sewers or watercourses.

As previously indicated in section 2.1, the Hatfield Business Park site currently has a site wide adopted foul and surface water drainage system that has previously been put in place to cater for discharges from the various undeveloped plots including this development – Plot 5000.

The proposal is for foul and surface water to discharge from Plot 5000 to the existing positive drainage spurs that have already been constructed from the main sewers within Mosquito Way to serve the development.

5.2 Proposed Drainage

The findings of the preliminary site investigation data confirms the prevailing ground conditions are made ground, silty clay or fine sands and gravels encountered from ground level and beyond.

The site infiltration confirms permeabilities varies from 3.13×10^{-6} m/s to 2.92×10^{-5} m/s which confirms low level of infiltration is possible in specific areas, previous communications with The Environment Agency have concluded the drainage of the site via soakaway methods is not preferred – hence the current Business Park drainage strategy that is in place.

Concerns have previously been raised that allowing surface water infiltrate into the ground may promote the mobilisation of deep historic contaminants below ground and this may lead to possible contamination of the underlying aquifer.

The above constraints should however not prohibit the incorporation of SUDS drainage techniques into the proposed drainage strategy.

A proposed levels and drainage strategy plan is included within Appendix B of this report that illustrates the various techniques that are to be adopted.

The development plot has the use of a surface water drainage spur emanating from the storm water sewer in Mosquito Way. The spur not only serves the proposed development it will also serve a future development plot to the east.

It is envisaged that the proposed new main building is to have a syphonic roof water drainage system.

The service yard will have an oversized surface water drainage channel to collect runoff and provide additional underground attenuation volume. It will discharge to the on-site storm water drainage system and cellular storage tank via a suitably sized Class 1 full retention oil interceptor.

Further attenuation volume is to be provided to the car parking area in the form of free draining sub-base. This is to minimise any flooding during extreme rain fall events.

The new area of staff and visitors car parking area will be constructed as an area of permeable surfacing that will comprise permeable block paving underlain by a suitable free draining subbase material that will enable surface water run-off to be attenuated. This design will help attenuate peak design flows from the development by utilising the volume available within the permeable stone (type 1 material with no fines) within the structural layers of the construction. It is proposed that the permeable stone media is tanked by an impermeable membrane and flows are allowed to discharge into the drainage system via a series of perforated pipes placed within the stone media.

These methods of surface water interception / collection will also avoid the need to provide oil interceptor units within parking areas as the stone media under the permeable block paving will naturally capture hydrocarbon contaminants.

5.2.1 Proposed Foul Drainage

An existing drainage spur has previously been constructed off the public sewer in Mosquito Way to serve this site.

The proposed foul drainage strategy for the new development anticipates Thames Water will allow the use of the historically dedicated spur to discharge foul flows into the public sewer within Mosquito Way.

5.3 PROPOSED SUDS MEASURES - SUMMARY

5.3.1 Ground Permeability (Soakaways)

The findings of the ground investigation report would seem to suggest variable permeability across the site and that infiltration drainage techniques directly into the underlying strata would not be appropriate for use as part of the surface water drainage strategy.

5.3.2 Allowable Surface Flooding

Additional storage of peak storm water can be facilitated by allowing car-parking and Service yard areas to flood up to a maximum of 100mm, provided this does not put the buildings, or neighbouring properties at risk of flooding. The proposed site levels will be set such that this is achieved, and will need to be carefully considered to ensure that flooding is routed away for the proposed new office / populated areas.

5.3.3 Filtration / Cleaning

There will be a natural filtering/cleaning out of any hydrocarbon pollution form the effect of surface water passing through the stone media underneath the permeable car parking surfacing. The use of a petrol interceptor is not proposed in this instance, although full retention interceptors will still be incorporated into the service yard drainage scheme.

5.3.4 Underground Storage

Underground attenuation storage is to be provided to the surface water drainage system in the form a cellular tank, oversized drainage channels may also be provided to provide additional storage volumes at times of the higher 1 in 100 year plus climate change storm return periods.

5.3.5 Flow Controls

Peak surface water discharge rate to the public sewer is to be controlled by the introduction of a vortex control device installed within the on outfall manhole to limit the discharge to the pro rata value of 57 l/s, which is based on a 1 in 100 year plus 30% climate change storm event.

5.3.6 Maintenance

The complete drainage system will have a detailed maintenance regime in place prior to occupation. This regime will involve an inspection after 3 and 6 months, and any maintenance required will be carried out. A further inspection will be carried out after 12 months, after which the maintenance schedule will be reviewed and adjusted to suit the circumstances and maintenance requirements of the development. In any case following severe storm events, the system will be inspected to ensure that all elements are performing satisfactory.

5.4 Drainage Design Summary

Taking onboard the techniques previously discussed the following features are proposed for the scheme drainage strategy:

- Introduce oversizing of surface water drainage channels within the plot to provide underground storage volume.
- Introduce a surface water control to limit the discharge rate from the new development into the existing Infrastructure sewer via a vortex control device.
- Provide cellular storage tank. This provide a very high percentage of storage volume and surface area given the space required; whilst they are deemed not to provide any form of hydrocarbon capture they generally provide an effective means of attenuation storage volume.
- Provide permeable paving to the proposed new vehicular parking areas, where applicable.
- Allowing the external car parks, service yard areas to flood in the more extreme 1 in 100 year plus 30% climate change storm events. (Underground storage is to be designed such that no flooding occurs at the 1 in 30 year event).
- Incorporate a full retention interceptor serving to the service yard surface water drainage system.

The above systems are illustrated with the drainage strategy plan 12313 / 106 within appendix B of this report.

5.4.1 Discharge Rates

The Hatfield Business Park drainage system had been sized to allow various developed and undeveloped plots certain restricted surface water peak discharge rate into it.

This 1.20 Ha undeveloped plot of land under consideration has previously been allocated a 100 year plus climate change pro rata allowable peak surface water discharge rate of 57 l/s. It is therefore proposed that this rate is used to limit peak discharge rate values to the surface water design. (Refer to microdrainage calculations in appendix C).

5.4.2 Windes Design Analysis

Microdrainage simulation calculations indicate a volume of 115m³ simulation of underground surface water attenuation is required for the 1 in 100 year return period plus 30% climate change to prevent the onset of any excessive flooding.

The proposal is for attenuation to be provided in the form of cellular crates, oversized channels and free draining sub base to car parking to help to control flood waters for the 1 in 100 year plus climate change event to ensure all flood waters are contained on the site.

The proposed development levels will be set such that any flooding is confined to the main service yard area. In storm water exceedance events routing will be applied to ensure protection to proposed buildings and adjacent landowners.

Drainage Strategy drawing and levels 12313 / 106 within Appendix B of this report also illustrates the potential flood routing.

Refer to Microdrainage simulation calculating within Appendix C of this report.

6 Summary

Baynham Meikle Partnership has prepared this Flood Risk Assessment along the lines set out in National Planning Policy Framework (NPPF) formerly Planning Policy Statement Note no. 25 (PPS25), and SUD's manual c753 to support this Outline Planning Application.

The Flood Risk Assessment may be summarised as follows:

- The Flood Maps have shown that the site is not identified to be at risk from fluvial flooding and does not form part of the functional floodplain.
- The surface water discharge rate from the development will be limited to historic agreed pro rata value such that the volume of storage available to this plot within the Hatfield Business Park drainage system is realised.
- The surface water runoff from the development site will be controlled. This is to be achieved through flow attenuation and the use of SUDS techniques in the new design. The techniques proposed are sub-surface storage in the way of cellular tanks, oversized channel and permeable surfacing lined / tanked infiltration structures.
- External area of service yard is to be allowed to temporarily flood by circa 100mm in extreme storm events. Finished ground levels will be carefully considered and flood routing will be applied to ensure protection proposed buildings and where possible adjacent landowners, in the event of extreme conditions.
- The water quality will also be improved because of the use of SUDS drainage techniques such as permeable surfacing.
- The quality of water discharging from site will be assisted by the incorporation of a Class 1 full retention petrol interceptor serves the proposed service yard.

It can therefore be said that the proposed development drainage scheme will not increase the potential of any flooding. This is mainly due to the peak runoff flows from the site being controlled and the adoption of recommended SUDS design techniques in line with the EA guidance.

APPENDIX A – EXISTING DRAWINGS

- 12313 / 100 SITE LOCATION PLAN
- 12313 / 101 TOPOGRAPHICAL SURVEY PLAN
- 12313 / 102 Environmental Agency Flood Map
- 12313 / 103 CONSTRAINTS PLAN





- WORKS BOUNDARY

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APPENDIX B – PROPOSED DRAWINGS

- 12313 / 104 PROPOSED SITE LAYOUT PLAN
- 12313 / 106 PROPOSED DRAINAGE STRATEGY PLAN
- 12313 / 110 PROPOSED IMPERMEABLE AREAS PLAN



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NOTES	A1
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PROPOSED IMPERMEABLE AREAS PLAN	
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Drawn byK.M.Checked byP.I.Project EngineerN.S.EDateScaleProject NoDrawing NoRevFEB20171:50012.31.3110-	J.
BAYNHAM MEIKLE Consulting Structural & Civil Engineers	
8 Meadow Road, Edgbaston, Birmingham B17 8BU Tel: 0121 434 4100 Fax: 0121 434 4073 Email: admin@bm-p.co.uk	

 $\underline{APPENDIX\ C-MICRODRAINAGE\ CALCULATIONS}$

- 12313 - Plot 5000 Simulation Calculations for Planning

aynham Meikle Partnership			Page 1
Meadow Road	Plot 5000		2
dgbaston, Birmingham	Hatfield Busin	ness Park	Ty .
5 1 / 8BU		n	Micro
ate 17 March 2017	Designed by P'	l' 2	Drainad
The 12313 Drainage for Plan	Checked by N.S	S.B.	
licro Drainage	Network 2016.	1	
STORM SEWER DESIGN	by the Modified	d Rational Me	thod
Design	Criteria for S	Storm	
Pipe Sizes ST.	ANDARD Manhole Siz	zes STANDARD	
FSR Rainfal	l Model - England	and Wales	
Return Period (years)	1 A	dd Flow / Climat	e Change (%) (
Ratio R	20.000	Maximum Backdro	p Height (m) 0.200
Maximum Rainfall (mm/hr)	0 Min Desig	n Depth for Opti	misation (m) 1.200
Maximum Time of Concentration (mins)	30 Min Ve	l for Auto Desig	n only (m/s) 1.00 sation $(1:x)$
rour sewage (I/S/Na)	0.750 Min	στοδε τοι οδιιψι	Bacion (1·A) 500
Volumetric Runoff Coeff.		C 1 .	
Volumetric Runoff Coeff.	1		
Volumetric Runoff Coeff. Desigr	ned with Level Sof	Ilts	
Volumetric Runoff Coeff. Desigr	ned with Level Sof	Ilts	
Volumetric Runoff Coeff. Desigr 	ned with Level Sof	r Storm	
Volumetric Runoff Coeff. Design <u>Network I</u> PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi	Design Table for E. Base Ins) Flow (1/s) (m	r Storm k HYD DIA S mm) SECT (mm)	ection Type Auto Desigr
Volumetric Runoff Coeff. Design <u>Network I</u> PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi 1.000 3.600 0.375 9.6 0.510 2	Design Table for E. Base Lns) Flow (1/s) (n	r Storm k HYD DIA S nm) SECT (mm) 600 o 375 P	ection Type Auto Design ipe/Conduit
Volumetric Runoff Coeff. Design <u>Network I</u> PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0	Design Table for E. Base Ins) Flow (1/s) (1 2.00 0.0 0. 0.00 0.0 0.	r Storm k HYD DIA So nm) SECT (nm) 600 o 375 P 600 o 300 P	ection Type Auto Design ipe/Conduit 🔒 ipe/Conduit 🔒
Volumetric Runoff Coeff. Design <u>Network I</u> PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0.0 0.0 0.00 0.0 0.0 0.0 0.00 0.0 0.0 0.0	r Storm k HYD DIA Somm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12	ned with Level Soft Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0.	r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length (m) Fall Slope I.Area T. (ha) T. (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0	r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) T. (m) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0	r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P 600 0 825 P	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0	r Storm k HYD DIA So mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 100 P 600 0 100 P 600 0 300 P 600 0 300 P 600 0 825 P ble	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0 Netw	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0. 0.00 0.0 0.	r Storm k HYD DIA So mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P 600 0 300 P 600 0 300 P 600 0 825 P cole	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0 Netw PN Rain T.C. US/IL E I.3 (mm/hr) (mins) (m)	Design Table for Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0. 0.00 <td< td=""><td>r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 100 P 600 0 300 P 600 0 825 P <u>olle</u> coul Add Flow V L/s) (1/s) (m</td><td>ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit</td></td<>	r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 100 P 600 0 300 P 600 0 825 P <u>olle</u> coul Add Flow V L/s) (1/s) (m	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) T. (m) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0 Netw PN Rain T.C. US/IL E I.J I.000 0.00 2.01 73.500 0 1.000 0.00 2.01 73.500 0	Design Table for E. Base Ins) Flow (l/s) (n 2.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 vork Results Tak Fase F a) Flow (l/s) (l 0.0	r Storm k HYD DIA So mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 100 P 600 0 300 P 600 0 300 P 600 0 825 P <u>ole</u> foul Add Flow V L/s) (l/s) (m	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0 Netw PN Rain T.C. US/IL E I.3 N N Main T.C. US/IL E I.3 N Rain T.C. US/IL E I.3 1.000	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. .510 0.0 0. .826 0.0 0.	r Storm k HYD DIA So mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P 600 0 300 P 600 0 300 P 600 0 300 P 600 0 825 P coll Add Flow V L/s) (l/s) (m 0.0 0.0 5 0.0 0.0 1 0.0 0.0 1	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ise/Conduit ise/Conduit ise/Conduit
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi) 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0 Netw Netw PN Rain T.C. US/IL E I. (mm/hr) (mins) (m) (h) 1.000 0.00 2.01 73.500 0 1.001 0.00 2.09 72.500 0 1.002 0.00 2.57 72.450 0	Design Table for Design Table for E. Base Ins) Flow (1/s) (r 2.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 2.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. 0.00 0.0 0. vork Results Tak Area E Base a) Flow (1/s) (1 .510 0.0 .770 0.0 .826 0.0	r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P 600 0 300 P 600 0 300 P 600 0 825 P 01e Coul Add Flow V L/s) (1/s) (m 0.0 0.0 5 0.0 0.0 1 0.0 0.0 1	ection Type Auto Design ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ipe/Conduit ise (1/s) (1/s) (1/s) .88 649.1 0.0 .38 97.4 0.0 .53 108.1 0.0
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0 Netw PN Rain T.C. US/IL E I.3 1.000 0.00 2.01 73.500 0 1.001 0.00 2.09 72.500 0 1.002 0.00 2.57 72.450<	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.100 0.0 0.0 0.100 0.0 0.0 0.100 0.0 0.0 .510 0.0 0.0 .125 0.0 0.0	r Storm k HYD DIA Sr mm) SECT (mm) 600 0 300 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P 601 0 0 0 S 601 0 0 0 5 0 0 0 0 1 0 0 0 0 2	ection Type Auto Design ipe/Conduit ipe/Co
Volumetric Runoff Coeff. Design Network I PN Length Fall Slope I.Area T. (m) (m) (1:X) (ha) (mi 1.000 3.600 0.375 9.6 0.510 2 1.001 6.500 0.050 130.0 0.260 0 1.002 44.400 0.420 105.7 0.056 0 2.000 12.300 1.770 6.9 0.125 12 1.003 54.600 0.475 114.9 0.002 0 1.004 14.300 0.048 297.9 0.000 0 Netw PN Rain T.C. US/IL E I.3 (mm/hr) (mins) (m) (ha) 1.000 0.00 2.01 73.500 0 1.001 0.00 2.07 72.450 0 2.000 0.00 12.07 74.000 0 1.003 0.00 12.69 72.030 0 <td>Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 vork Results Tak Tak Area E Base F a) Flow (1/s) (1 1 .510 0.0 0.0 .826 0.0 0.0 .125 0.0 0.0</td> <td>r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P 600 0 300 P 600 0 300 P 600 0 825 P 01e Coul Add Flow V l/s) (l/s) (m 0.0 0.0 5 0.0 0.0 1 0.0 0.0 1</td> <td>ection Type Auto Desigr ipe/Conduit ipe/Co</td>	Design Table for E. Base Ins) Flow (1/s) (n 2.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 0.00 0.0 0.0 vork Results Tak Tak Area E Base F a) Flow (1/s) (1 1 .510 0.0 0.0 .826 0.0 0.0 .125 0.0 0.0	r Storm k HYD DIA S mm) SECT (mm) 600 0 375 P 600 0 300 P 600 0 300 P 600 0 100 P 600 0 300 P 600 0 300 P 600 0 300 P 600 0 825 P 01e Coul Add Flow V l/s) (l/s) (m 0.0 0.0 5 0.0 0.0 1 0.0 0.0 1	ection Type Auto Desigr ipe/Conduit ipe/Co

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Baynham Meikle Partnership		Page 3
8 Meadow Road	Plot 5000	
Edgbaston, Birmingham	Hatfield Business Park	L
B 17 8BU		Micco
Date 17 March 2017	Designed by PT	Desinado
File 12313 Drainage for Plan	Checked by N.S.B.	Diamaye
Micro Drainage	Network 2016.1	

Synthetic Rainfall Details

Rainfall Model		FSR		Profile Type	Summer
Return Period (years)		1		Cv (Summer)	0.750
Region	England	and Wales		Cv (Winter)	0.840
M5-60 (mm)		20.000	Storm	Duration (mins)	30
Ratio R		0.400			

Baynham Meikle Partnership					Page 4
8 Meadow Road	Plot F	5000			
Edgbaston. Birmingham	Hatfie	eld Busir	less Park		4
B 17 8BII	macric				1 mm
Date 17 March 2017	Degiar	hed by DT	۰ ۲		Micro
Eile 12212 Drainage for Dian	Chook		סיי		Drainage
File 12313 Drainage for Plan	. Checke		.в.		,
Micro Drainage	Networ	CK 2016.1	-		
Onlin	e Contro	le for S	torm		
		15 101 5			
Hydro-Brake Optimum® Man	hole: 4,	DS/PN:	1.003, Vo	lume (m³)	: 7.3
Unit Reference Design Head (m)			MD-SH	E-0273-5700	3 720-5700
Design Flow (1/s)					57.0
Flush-Flo™					Calculated
Objective			Mini	mise upstre	eam storage
Application					Surface
Diameter (mm)					res 273
Invert Level (m)					72.030
Minimum Outlet Pipe Diameter (mm)	Site Spea	cific Desi	gn (Contact	Hydro Inte	ernational)
Suggested Manhole Diameter (mm)	Site Spec	cific Desi	gn (Contact	Hydro Inte	ernational)
Control	Points	Head (r	n) Flow (1/s	5)	
Design Point	Calculate	d) 3.72	20 56	.9	
	Flush-Fl	o™ 1.05	73 56	.9	
	Kick-Fl	o® 2.22	28 44	. 5	
Mean Flow over	Head Ran	ge	- 49	. 8	
The hydrological calculations have	heen has	ed on the	Head /Discha	rae relatio	onghin for the
Hydro-Brake Optimum® as specified.	Should a	another ty	pe of contr	ol device of	other than a
Hydro-Brake Optimum® be utilised t	hen these	storage r	outing calc	ulations wi	ill be
invalidated					
Depth (m) Flow (1/s) Depth (m) F	.ow (1/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100 8.6 1.200	56.8	3.000	51.3	7.000	77.3
0.200 28.1 1.400	56.1	3.500	55.3	7.500	80.0
0.300 44.5 1.600	54.9	4.000	59.0	8.000	82.5
0.400 48.7 1.800	53.0	4.500	62.4	8.500	85.0
	50.0 45 4	5.000	65.7	9.000	87.4
0.000 33.7 2.200	46.1	6.000	71.8	5.500	09.7
0.800 56.1 2.400					
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6	I	
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
0.800 56.1 2.400 1.000 56.9 2.600	47.9	6.500	74.6		
	47.9	6.500	74.6		

Baynham Meikle Partnership		Page 5
8 Meadow Road	Plot 5000	
Edgbaston, Birmingham	Hatfield Business Park	4
B 17 8BU		- m
Date 17 March 2017	Designed by PT	MICLO
File 12313 Drainage for Plan	Checked by N S B	Drainage
Micro Drainage	Network 2016 1	
	Network 2010.1	
Storage	Structures for Storm	
<u>Cellular Stora</u>	ge Manhole: 2, DS/PN: 1.001	
Inver Infiltration Coefficient Infiltration Coefficient	t Level (m) 72.500 Safety Factor 2.0 Base (m/hr) 0.00000 Porosity 0.95 Side (m/hr) 0.00000	
Depth (m) Area (m²) Inf. Are	ea (m²) Depth (m) Area (m²) Inf. Area	(m²)
0.000 115.0	115.0 1.000 115.0 15	57.9
Porous Car Par	k Manhole: 4, DS/PN: 2.000	
Infiltration Coefficient Base	(m/hr) 0.00000 Width (m)	68.8
Membrane Percolation ((mm/hr) 1000 Length (m)	15.6
Max Percolation	n (l/s) 298.1 Slope (1:X)	30.0
Safety	Factor 2.0 Depression Storage (mm)	5
Invert Lev	vel (m) 74.500 Evaporation (mm/day)	3
		-

Baynham Meikle Partnership P											
8 Meadow Road	Plot 5000										
Edgbaston, Birmingham	Hatfield Business Park	Ly									
B 17 8BU		Micro									
Date 17 March 2017	Designed by PT	Drainago									
File 12313 Drainage for Pla	n Checked by N.S.B.	Diamage									
Micro Drainage	Network 2016.1										
Summary of Critical Re	sults by Maximum Outflow (Rank 1	L) for Storm									
Baysham Meikle Partnership Page 6 3 Meadow Road Bdgbaston, Birningham Hatfield Business Park a 17 March 2017 Designed by PT Date 17 March 2017 Designed by PT The Reduction Partner Checked by N.S.B. Micro Drainage for Plan Checked by N.S.B. Micro Drainage metwork 2016.1 Summary of Critical Results by Maximum Outflow (Rank 1) for Storm <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Summary of Critical Results by Maximum Outflow (Rank 1) for Storm</u> <u>Bistical Reduction Pactor 1:000 Additional Flow - % of Total Plow 0.000</u> Rot Start Laval (mm) 0 MADD Factor 1:0m/As Storage 2.000 Number of Offline Controls 0 Number of Storage Structures 2 Runber of Offline Controls 0 Number of Storage Structures 2 Number of Offline Controls 0 Number of Storage Structures 2 Number of Offline Controls 0 Number of Time/Arae Dagrams 0 Number of Offline Controls 0 Number of Eal Time Controls 0 <u>Synthetic Rainfail Details</u> Nanlysis Timestep Fine Inertia Status OFF Duration(a) (mins) 15, 30, 60, 120, 180, 240, 360, 440, 600, 720, 90, 1446, 2160 Not 1 Status 0N <u>Profile(s)</u> (years) 1. 30, 100 Climate Change (N) 000 1.50 Not 30/15 Summer 1.001 1 15 Summer 100 +308 10/15 Summer 1.001 1 15 Summer 100 +308 10/15 Summer 1.001 1 15 Summer 100 +308 30/15 Summer 1.001 1 74.490 Name (mm) (m) (a ³ Cap. (1/a) Nitter 1.001 1 74.490 Name (m) (m) (a ³ Cap. (1/a) (1/a) Status Exceeded 1.001 1 74.490 1.001 1 74.490 Name (mm) (m) (a ³ Cap. (1/a) (1/a) Sta											
Number of Input H Number of Onlin Number of Offlin	ydrographs 0 Number of Storage Structu e Controls 1 Number of Time/Area Diagr e Controls 0 Number of Real Time Contr	res 2 ams 0 ols 0									
Rainfall Mod Regi	Synthetic Rainfall Details el FSR Ratio R 0.400 on England and Wales Cv (Summer) 0.750										
M5-60 (m	n) 20.000 Cv (Winter) 0.840										
Margin for Flood	Risk Warning (mm) 150.0 DVD Status Analysis Timestep Fine Inertia Status DTS Status ON	3 ON 3 OFF									
Profile Duration(s) (mir	s) Summer a s) 15, 30, 60, 120, 180, 240, 360, 720, 960, 1	and Winter 480, 600, 1440, 2160									
Return Period(s) (year Climate Change (s) . %)	1, 30, 100 0, 0, 30									
US/MH Return PN Name Storm Period	Climate First (X) First (Y) F Change Surcharge Flood (first (Z) Overflow Overflow Act.									
1.000 1 15 Summer 100	+30% 100/15 Summer										
1.001 2 30 Summer 100	+30% 30/15 Summer										
1.002 3 15 Summer 100	+30% 30/15 Summer 100/120 Winter										
1.003 4 15 Winter 30	+0% 30/15 Summer +30% 1/15 Summer										
1.004 5 30 Summer 100	+30%										
Water Surchard	ed Flooded Pipe										
US/MH Level Depth	Volume Flow / Overflow Flow	Level									
PN Name (m) (m)	(m ³) Cap. (l/s) (l/s) St.	atus Exceeded									
1.000 1 74.489 0.0	14 0.000 1.58 378.6 SURC	HARGED									
1.001 2 74.170 1.1	70 0.000 1.54 94.3 SURC	HARGED									
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	YU U.UUU U.80 81.1 SURC 53 0.000 0.97 21.3 STEC	HARGED									
1.003 4 74.491 2.1	61 0.000 0.58 56.8 SURCE	HARGED									
1.004 5 71.201 -0.	49 0.000 0.10 56.8	OK									
	1982-2016 XD Solutions										
	2202 2010 ML DOTACTOID										

 $\underline{APPENDIX} \ \underline{D} - \underline{SITE} \ \underline{INVESTIGATION}$

- RSK TRIAL PITS EXPLORATORY LOCATION PLAN
- TRIAL PIT LOGS
- SOAKAWAY TESTS
- CBR % TESTS

Contract Re	ef:			Start:	06.0	3.17	Ground Level:	Co-ord	dinates:	Sheet:						
	313	555		End:	06.0	3.17		-1.2.9			1	of 1				
Sam	ples a	nd In-s	itu Test	s	ter	(III)		25.15	1.7.1.2.1.1.		Depth	Materi				
Depth	No	Туре	Re	sults	Wa	Bac		Descrip	tion of Strata		(Thick ness)	Legen				
0.20 0.20 0.40 0.40 0.50	1 2 3	ES PID ES PID B	0.0 0.0	oppm oppm			Grass over brown and rootlets. Sand coarse quartzite an \(TOPSOIL) Firm to stiff brown coarse. Gravel is a (LOWESTOFT FO	slightly grave is coarse. Gr id flint. slightly grave ngular to sub- RMATION)	elly clayey SAND wit avel is sub-angular to elly silty sandy friable -angular fine to coarse	h frequent roots o rounded fine to e CLAY. Sand is e flint.	0.25					
1.00 1.00 1.00	4 5	00>	c _u =82/8	89/92/90			becoming mor	gl.	- -(1.55) -							
_	2	1								1	1.80					
1.80	7	D				Light orangish brown gravelly very clayey SAND with frequent pockets of clay. Sand is fine to coarse. Gravel is angular to sub-rounded fine to coarse flint. (LOWESTOFT FORMATION)										
3.00	8	D									3.10	6 P				
3.20 3.20	9	D V	c _u =55	5/52/50			and grey silty rounded fine to	(0.70)								
0.70											-	× - ×				
3.70 10 D							Trial pit terminated	at 3.80m bgl.								
											ł					
Plan (Not to	2.00 →						General Remarks 1. Location scanned with GPR and a CAT and signal generator prior to breaking ground. No services detected. 2. Trial pit remained stable during excavation. 3. Groundwater not encountered. 4. Trial pit backfilled with arisings upon completion. 5. UXO specialist present onsite observing the excavation of the trial pit for UXO mitigation									
						- 210	All dimensions in m	netres	Scale:	1:28						
Method	-			Plant	t 1.		100 207	Logged Checked								

Contract Re	ef:	1	5	Start:	06.0	3.17	Ground Level:	Co-ord	linates:	Sheet		0.5 1 5 1					
	3135	555	E	End:	06.0	3.17					1	of 1					
Sam	ples a	nd In-sit	u Tests	-	ter	kfill					Depth	Materia					
Depth	No	Туре	Resu	lts	Wa	Bac		Descrip	tion of Strata		(Thick ness)	Legen					
0.10 0.10	1	ES PID	0.0pp	m			Grass oer light br roots and rootlets sub-rounded fine to \(TOPSOIL)	own slightly . Sand is fin coarse quar	gravelly clayey SAN ne to coarse. Grav Izite and flint.	ID with frequent el is angular to	(0.30) 0.30	14 24 X					
0.40 0.50 0.50 0.60 0.60	2 3 4	B PID D V	0.0pp c _u =30/5	m 5/60			Firm light orangisl CLAY. Sand is fine coarse flint. (LOWESTOFT FO	n brown to b to coarse. Gi RMATION)	prown slightly gravel ravel is angular to su	ly slightly sandy b-rounded fine to	(1.10)						
1.00 1.00	5	D V	c _u =55/5	7/60													
1.30	6	D									1.40	0					
1.50	7	В				Orange brown slightly silty clayey very gravelly SAND. Sand is coarse. Gravel is sub-angular to sub-rounded fine to coarse flint. (LOWESTOFT FORMATION)											
2.00	8	D					Cobbles of flin	t from 2.00m	bal.		-						
							Orange brown sli	abtly silty da	avev very sandy GE	RAVEL Sand is	2.20	0-0					
3.00	9	D									(0.90)	1016 1010					
Plan (Not to	Scal	e)						Gener	ral Remarks		-						
1.00							 Location scanned with GPR and a CAT and signal generator prior to breaking ground. No services detected. Trial pit sidewalls were unstable from 2.00m bgl, thus trial pit was terminated at 3.10m bgl. Groundwater not encountered. Trial pit backfilled with arisings upon completion. UXO specialist present onsite observing the excavation of the trial pit for UXO mitigation purposes. 										
							All dimensions in m	atura .	Cooler	1.20	-	_					
								leires	Scala	1.70							

Contract Re	f:	math	Jiul	Start	06.0	3 17	Ground Level	Co-ord	linates:	Sheet		5/100	
Sonnaotine	3135	55		End	06.0	3.17		00-010		Grieet	1	of 1	
Same	les an	d In-situ	Tests		1	=					Depth	Materi	
Depth	No	Type	Res	sults	Wate	Backfi		Descrip	tion of Strata		(Thick ness)	Graph	
0.20 0.20 0.30 0.30 0.60	1 2 3 4	ES PID B D ES	0.0¢	opm			Firm brown slightl rootlets. Sand is coarse quartzite, fl (MADE GROUND) Stiff to very stiff lig gravelly, silty CLA	ly gravelly sar coarse. Grave lint, brick, cond) ght orangish b Y. Gravel is a	ndy CLAY with occa el is angular to sub crete, wire, flagstones rown occasionally lig ingular to sub-rounde	sional roots and -rounded fine to s and cloth. The brown slightly ed fine to coarse	(0.50) 0.50		
0.60 0.80 0.90	5	PID B D	0.0p	mqc			flint. (LOWESTOFT FC	RMATION)			-(0.60)		
1.00	7	D					Trial nit terminated	for soakaway	testing at 1 10m hal		1.10	<u>_o</u>	
Plan (Not to	an (Not to Scale)						on scanned with GPR	Genei R and a CAT ai	ral Remarks	prior to breaking gr		0	
	<u> </u>			1	 Grounowater not encountered. Trial pit backfilled with arisings upon completion. UXO specialist present onsite observing the excavation of the trial pit for UXO mitig purposes. 								
							All dimensions in n	netres	Scale:	1:28			

Contract Re	ef:	,		Start:	06.0	3.17	Ground Level:	Co-ore	dinates:	Sheet:		
	313	555		End:	06.0	3.17					1	of 1
Sam	ples a	nd In-sit	u Test	s	er	II.			3.3.5.5.3.		Depth	Mater
Depth	No	Туре	Res	sults	Wat	Back		Descrip	otion of Strata		(Thick ness)	Graph
0.10 0.10 0.10	1 2	ES D PID	0.0	ppm			Grass over dark br fine to coarse. Gr quartzite and flint v (POSSIBLE MADE	own slightly o avel is sub-a vith rare brick GROUND)	clayey, slightly gravell angular to subrounde fragment.	y SAND. Sand is d fine to coarse	0.20	
0.40 0.40 0.50	3 4	es Pid D	0.0	ppm			Firm light orangish is coarse. Gravel is (LOWESTOFT FO	brown slight angular to s RMATION)	lly gravelly slightly sa ub-rounded fine to co	ndy CLAY. Sand arse flint.	-	
1.00 1.00	5	B V	c _u =50	1/59/47				- (1.45) - -				
1.60	6	D				Orange brown slightly silty clayey very gravelly SAND. Sand is fine to coarse. Gravel is angular to sub-rounded fine to coarse flint. (LOWESTOFT FORMATION) Becoming more yellowish brown from 1.80 to 2.50m bgl.						
2.00	7	D										
											(1.45)	
3.00	8	D					Sand become:	a damp from 3	3.00m bgl.		3.10	-
			D Sand becomes damp from 3.00m bgl. Trial pit terminated at 3.10m bgl due to sidewalls collapsing fr 2.50m bgl.									
			-		-	Ļ				4		
Plan (Not to 00.		e) — 2.00) —•]	1. L s 2. T 3. C 4. T 5. U	ocatic service Frial pi Ground Frial pi JXO s purpos	on scanned with GPR es detected. t sidewalls were unsta dwater not encountere t backfilled with arisin pecialist present onsi es.	Gene and a CAT a able from 2.5 ad. gs upon com te observing t	ral Remarks and signal generator p 0m bgl, thus trial pit w apletion. the excavation of the	prior to breaking gr vas terminated at 3 trial pit for UXO m	ound. No 3.10m bg itigation	0 اار
							All dimensions in m	etres	Scale:	1.28	-	
	athed				t			Logge	1	Checked		

Contract R	ef:			Start:	06.0	3.17	Ground L	evel:	Co-ord	inates:	Sheet	-			
	313	555		End:	06.0	3.17	1.47	1 <u></u>				1	of 1		
Sam	ples a	nd In-situ	u Test	s	ater	ckfill	1		Descript	tion of Strata		Depth (Thick	Mater		
Depth	No	Туре	Re	sults	3	Ba						ness)	Leger		
0.20 0.20 0.40 0.40 0.50	1 2 3	es Pid Es Pid B	0.0 0.0	ppm ppm			A construction of the cons	over brown s otlets. Sand ndec fine to c DIL) rk orangish I se. Gravel is a STOFT FOR	brown slight angular to su MATION)	by clayey SAND will coarse. Gravel is zite and flint. ly gravelly sandy CL ib-rounded fine to co	AY. Sand is fine barse flint.	(0.30) 0.30 (0.90)			
1.00 1.00	4 5	D D													
1.50	6	в					Light or coarse. occasio (LOWE	rangish brow Gravel is a nal pockets c STOFT FOR	n clayey ve ingular to si of clay. MATION)	ery sandy GRAVEL.	Sand is fine to caorse flint with	-	P.01. 1.0 0.10		
2.00	7	D										(2.10)	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
2.50	8	D											10 10 10 10		
3.00	9	D										3.30	1. P. J. A. J.		
						Trial pit terminated at 3.30m bgl.									
Plan (Not te	o Scal	e)							Gener	al Remarks					
1.00	‡ [— 2.00	_]	1. L 2. 1 3. 0 4. 1 5. 0	Locatic Service Frial pi Ground Frial pi UXO s Durpos	on scanned s detected t remained dwater see t backfilled pecialist p es.	d with GPR a d. d stable during page encour d with arisings resent onsite	nd a CAT ar g excavatior ntered from 3 s upon comp observing th	nd signal generator p 3.10m bgl. oletion. ne excavation of the	prior to breaking gr	round. N	D		
							All dime	nsions in me	tres	Scale:	1:28				
Method			1	Plan	t d·			CY	Logged By:	MSouthworth	Logged Checked				

Plot	5000	, Hat	field	Busir	ness	s Par	k	Go	odmans		TP06	SA0
Contract Re	əf:	1.1	1.71	Start:	06.0	3.17	Ground Level:	Co-c	ordinates:	Sheet		
	3135	555		End:	06.0	3.17		1.1.1			1	of
Sam	ples a	nd In-si	itu Test	s	ater	ickfill		Desci	ription of Strata		Depth (Thick	Mate
Depth	No	Туре	Re	sults	3	ň	0	1. K		/	ness)	Leg
0.30 0.30 0.40 0.50	1 2 3	ES PID B D	0.0	ppm			Grass over dar roots and root sub-roundec fir (TOPSOIL) Light orangish Gravel is angul (LOWESTOFT	thets. Sand is ne to coarse qu brown clayey s ar to sub-round FORMATION)	y gravely sandy CLA fine to caorse. Grav artzite. sandy GRAVEL. Sand led fine to coarse flint.	is fine to coarse.	- 0.15 - - - - (0.65)	P.01. 1. 9 p
							Very stiff light of gravelly silty C	orangish browr LAY. Gravel is	n occasional mottled lig angular to sub-round	ght brown slightly ed fine to coarse	0.80	0
1.00	4	D	c =90/	120/120			flint. (LOWESTOFT	FORMATION)			+(0.40)	· · ·
1.10	5	Ď	Uu-90/	120/120			Trial pit termina	ted at 1.20m b	gl due to soakawav tes	ting.	1.20	
Dian (Mat 4	Plot 5000, Hatfield Bu intract Ref: S Samples and In-situ Tests Depth No Type Result 30 1 ES 90 2 B 50 3 D 00 4 D 5 D 00 4 Cu=90/120 10 5 D cu=90/120 an (Not to Scale) 00 0 01 4 D 01 5 D 00 0 01 5 D 00 0 00							Goo	aral Pamarka			
0. -		e) 2.0	0 —•]	1. L 2. 1 3. (4. 1 5. U	Location Service Frial pi Ground Frial pi JXO s Durpos	n scanned with G s detected. t remained stable water not encour t backfilled with an pecialist present c es.	PR and a CAT during excavat ntered. risings upon co onsite observing	and signal generator p tion. mpletion. g the excavation of the	prior to breaking gr trial pit for UXO m	round. N	0
					1		All dimensions	in metres	Scale:	1:28		1-
1 - 11 I	I F				t			Logg	ed	Checked		

Contract Re	ef:	, main		Start:	06.0	3.17	Ground Level:	Co-ord	linates:	Shee			-
	3135	555		End:	06.0	3.17		00 010			1	of	í.
Sam	ples a	nd In-situ	u Test	s	5	=			1		Depth	Mate	eri
Depth	No	Туре	Re	sults	Wat	Back	1.1.1.2.	Descrip	tion of Strata		(Thick ness)	Grap	en en
0.20 0.20 0.20 0.40	1 2 3	ES D PID B	0.0	ppm			Dark brown slighty and rootlets. Sand coarse quartzite wi (POSSIBLE MADE Light orangish bro	d gravelly slig d is fine to d th a rare piece GROUND). wn clayey gra	oarse. Gravel is sub oarse. Gravel is sub e of plastic meshing. avelly SAND. Sand i	th frequent roots b-angular fine to s fine to coarse.	(0.30) 0.30 0.50		
0.90	4	D				(LOWESTOFT FORMATION) Firm light orangish brown slightly gravelly sandy CLAY. Sand is fine to coarse. Gravel is angular to sub-rounded fine to coarse flint. (LOWESTOFT FORMATION)							
											1.50		11
1.60	6	в					Light orangish bro Gravel is angular to (LOWESTOFT FO	wn slightly cla o sub-rounded RMATION)	ayey gravelly SAND. d fine to coarse flint.	Sand is coarse.	-	0 4	1
2.00	7	D									(1.10)	\$ 4 4	A B C C
							Orange brown sligtbly sitty clavey year sandy GRAVEL Sand is						
2.80	8	D				Orange brown sligthly silty clayey very sandy GRAVEL. coarse. Gravel is sub-angular to sub-rounded fine to coarse f (LOWESTOFT FORMATION) becoming damp from 2.60m bgl.					- (0.70)	P.01. 1.9	
3.20	9	D									3.30	0.0	7
				-							F		
Plan (Not to	Scal	e)						Gene	ral Remarks	2			
1.00		2.00]	1. L 2. T 3. C 4. T 5. L	ocatio ervice frial pi Ground frial pi JXO s purpos	on scanned with GPR as detected. t remained stable dur dwater not encounter t backfilled with arisin pecialist present onsi es.	and a CAT a ing excavatio ed. gs upon com te observing t	nd signal generator p n. pletion. he excavation of the t	rior to breaking g trial pit for UXO n	round. N nitigation	D	
							All dimensions in m	netres	Scale:	1:28			-
Aethod Plant				Plan	t	Logged Checked							1

Plot 5000, Hatfield Busin					ness	ess Park Goodmans					TP08/SA08		
Contract Ref: Start: Start: End:				06.0	06.03.17 Ground Level:			Co-ordinates:	Sheet	Sheet:			
				06.0	3.17		8			1	of 1		
Samples and In-situ Tes			tu Test	S	ater	ckfill	Description of Strata			Depth (Thick	Materi Graph		
Depth	No	Туре	Results		N	Ba		Description of Strata			ness)	Legen	
0.10 0.10 0.30 0.30 0.50	1 2 3	ES PID ES PID D	0.0ppm 0.0ppm				Grass over brown slightly gravelly clayey SAND with frequent roots and rootlets. Sand is fine to coarse. Gravel is angular to sub-angular fine to coarse quartzite and occasional flint. (TOPSOIL) Firm to stiff brown slightly gravelly silty sandy friable CLAY. Sand is coarse. Gravel is angular to sub-abgular fine to coarse flint. (LOWESTOFT FORMATION)				- 0.15		
1.00	ā	в									F	<u></u>	
								inated at 1.2	om og for soakaway testin	g.			
											- 81 - 1		
			-		1								
rian (Not te	o scal	e)			11	ocatio	n scanned with	h GPR and a		prior to breaking a	round N	0	
1.00	1	2.00) — (]	2. 1 3. 0 4. 1 5. U	Frial pi Frial pi Frial pi JXO s	s detected. remained stal lwater not ence backfilled with pecialist presen- es.	ble during ex ountered. h arisings up nt onsite obs	cavation. on completion. erving the excavation of the	e trial pit for UXO n	nitigation		
					All dimensions in metres Scale: 1:28								
Method Plan					nt d				Logged	Checked			

STRUCTURAL SOILS LTD

INSITU TESTING REPORT

1774

Report No.	747205R.01(00)				
Date Client Address For the Atte	14-March-2017 RSK Environment Ltd Spring Lodge 172 Chester Road Helsby Cheshire WA6 0AR ntion of Melissa	Contract Plot 50	00, Hatfield		
Order receiv Testing Star Testing Con	red ted npleted	28-February-2017 10-March-2017 10-March-2017	Client Reference Client Order No. Instruction Type	None PO266043 Written	
Laboratory. UKAS Accr Not UKAS . 3no. Insitu	edited Tests Accredited Tests soakaway tests carried out at	t locations specified by cl	ient.		
The results 1	represent the ground condition	ons at the specified location	ons and depths at the time	of testing.	
Please Note: Test were und Opinions and	Remaining samples will be reta lertaken on samples 'as received interpretations expressed in thi	ined for a period of one mor d' unless otherwise stated. is report are outside the scop	ith from today and will then be of accreditation for this lab	be disposed of. poratory.	
Struct	ural Soils Ltd 1a Princess Stree	et Bedminster Bristol BS3 4/	AG Tel.0117 9471000. e-mai	il dimitris.xirouchakis@s	oils.co.uk

Page 4 of 4

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_015 Pryversion: v8_06 - Core+Logs - 002 | Graph I - DCP - 2 - CBR VALUE VS DEPTH - A4P | 313555 - PLOT 5000, HATFIELD BUSINESS PARK, 3PU - v8_06, | 14/03/17 - 10:00 | DM1 |

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_015 Pryversion: v8_06 - Core+Logs - 002 | Graph I - DCP - 2 - CBR VALUE VS DEPTH - A4P | 313555 - PLOT 5000, HATFIELD BUSINESS PARK, 3PU - v8_06, | 14/03/17 - 10:00 | DM1 |

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_015 Pryversion: v8_06 - CorretLogs - 002 | Graph I - DCP - 2 - CBR VALUE VS DEPTH - A4P | 313555 - PLOT 5000, HATFIELD BUSINESS PARK, 3PU - v8_06, | 14/03/17 - 10:00 | DM1 |

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_015 Pryversion: v8_06 - CorretLogs - 002 | Graph I - DCP - 2 - CBR VALUE VS DEPTH - A4P | 313555 - PLOT 5000, HATFIELD BUSINESS PARK, 3PU - v8_06, | 14/03/17 - 10:00 | DM1 |

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_015 Pryversion: v8_06 - CorretLogs - 002 | Graph I - DCP - 2 - CBR VALUE VS DEPTH - A4P | 313555 - PLOT 5000, HATFIELD BUSINESS PARK, 3PU - v8_06, | 14/03/17 - 10:00 | DM1 |

GINT_LIBRARY_V8_06.GLB LIbVersion: v8_06_015 Pryversion: v8_06 - Core+Logs - 002 | Graph I - DCP - 2 - CBR VALUE VS DEPTH - A4P | 313555 - PLOT 5000, HATFIELD BUSINESS PARK, SPU - v8_06, | 14/03/17 - 10:00 | DM1